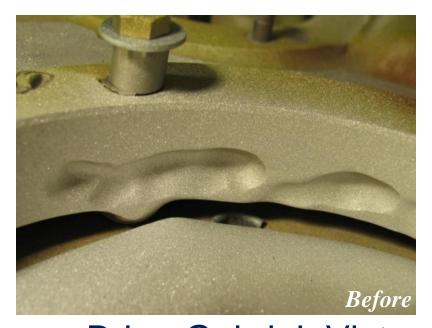
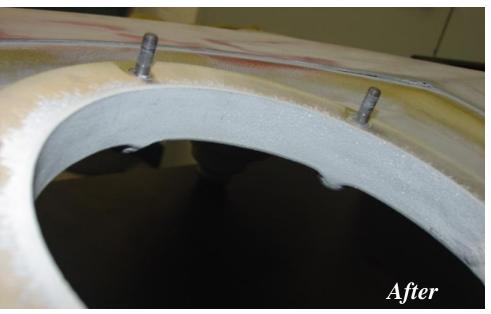






## Cold Spray for Repair of Magnesium Gearboxes





Brian Gabriel, Victor Champagne, Matt Trexler, Dennis Helfritch

ARL Center for Cold Spray

8 February 2011

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## Technical Objectives



Demonstrate and qualify cold spray aluminum alloy coatings which provide surface protection and a repair/rebuild methodology for Mg alloy components on Army and Navy helicopters and advanced fixed-wing aircraft such as the Joint Strike Fighter

#### 1.Cost-effective

#### 2.ESOH-acceptable technology





**MOUNTING FEET** 

MAIN GEARBOX

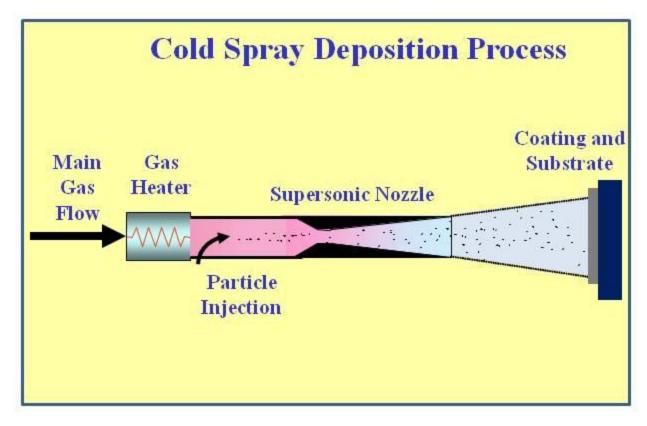


# Technical Approach



#### Cold Spray Process

Unique solid-state deposition process which utilizes high velocity particles impinging upon a substrate to build up material



- •Feed stock typically ranges from 1 to 50 μm
- •Particle ductility is crucial
- •Gas temperature range from R.T. to 800°C
- •No melting of particles
- •Negligible oxidation
- •No decomposition or phase changes of deposited particles or substrate

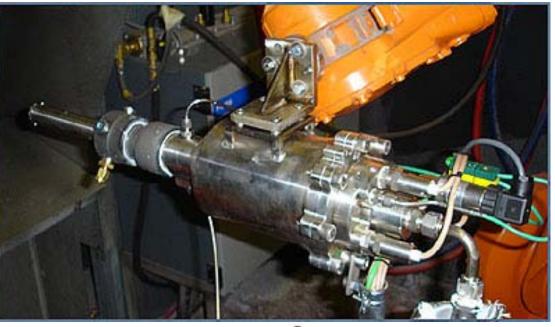
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# COLD SPRAY EQUIPMENT at FRC EAST









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## TECHNICAL APPROACH



#### Joint Test Protocol

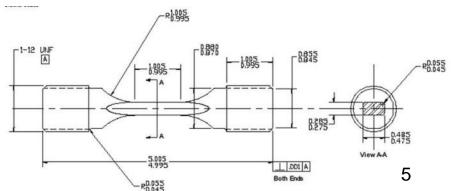
#### **Mechanical Tests**

- Adhesion Tensile Bond Test (ASTM C633)
- XRD Residual Stress
- R.R. Moore RB Fatigue
  - surface finished 125 R<sub>A</sub>
- Fretting Fatigue UTRC
- Impact ASTM D5420
- Hardness
- Porosity
- Triple Lug Shear

#### **Corrosion Tests**

- ➤ Un-scribed ASTM B117
- > Scribed ASTM B117
- > GM9540 Scribed
- ➤ Galvanic Corrosion (G71)
- Crevice Corrosion (G78)
- > Beach Corrosion
- ▶ G85 Annex 4-SO<sub>2</sub>

Stack Up: RockHard, 23377, and 85285



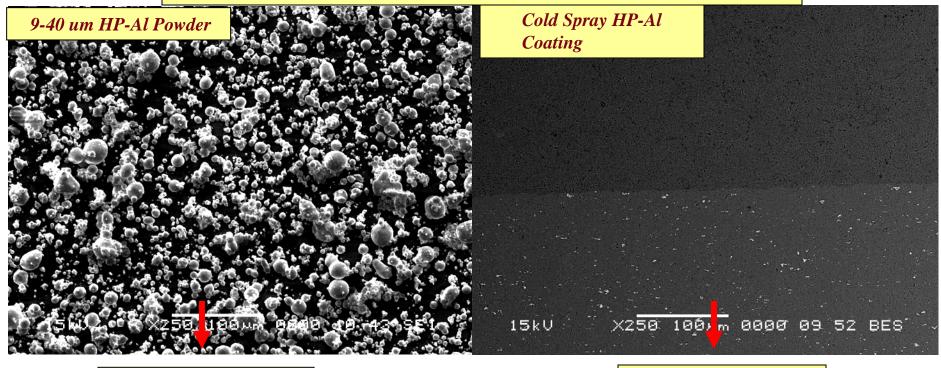
UTRC Fretting Fatigue Specimen



## Powder vs. Coating



# Oxygen content measured by Inert Gas Fusion ASTM E 1019-03



0.88 %Oxygen

CGT system

0.58 %Oxygen

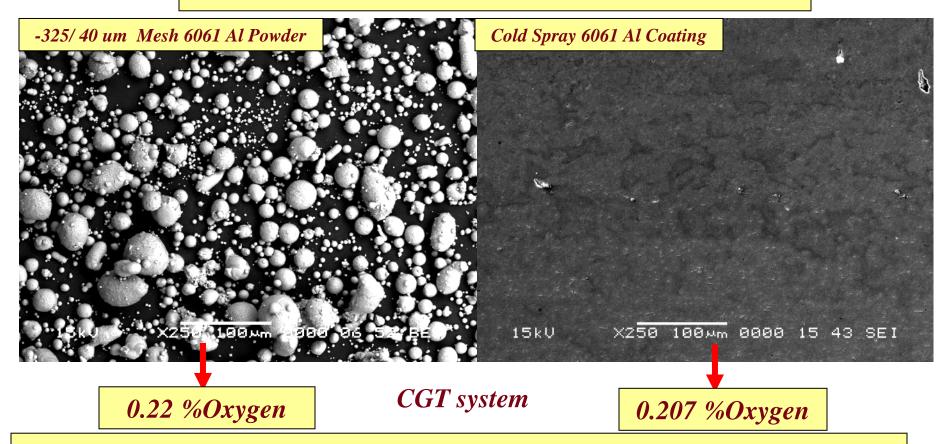
\*The oxygen content of the cold spray coating is largely determined by the oxygen content of the original powder, not the process.



## Powder vs. Coating



# Oxygen content measured by Inert Gas Fusion ASTM E 1019-03

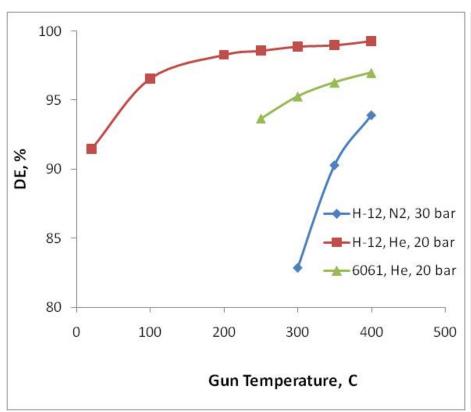


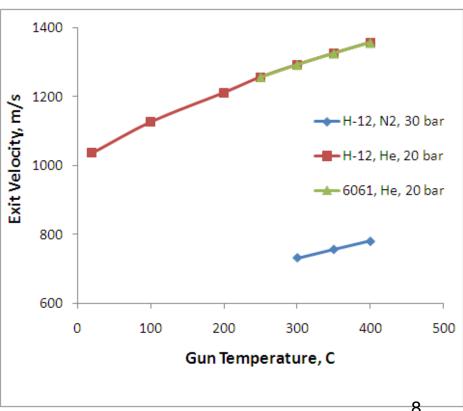
\*The oxygen content of the cold spray coating is largely determined by the oxygen content of the original powder, not the process.





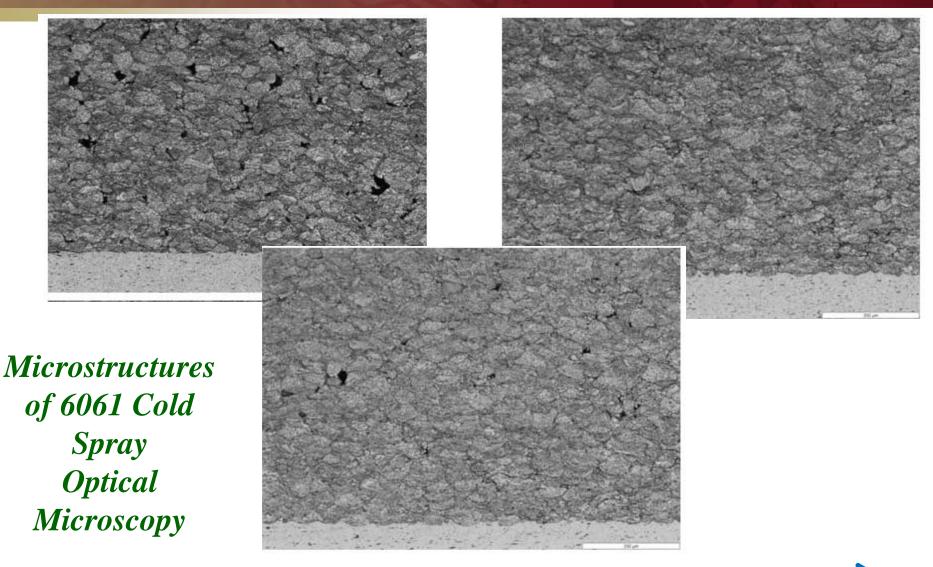
Modeled deposition efficiencies appear to be close to experimental values while the calculated velocities are well above the critical velocities for Al (~500 m/s)







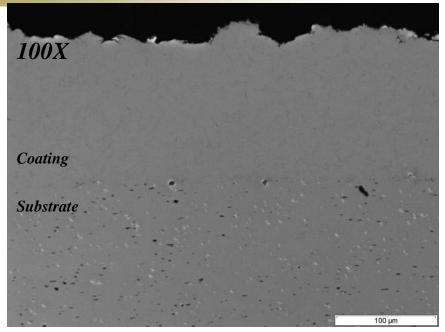


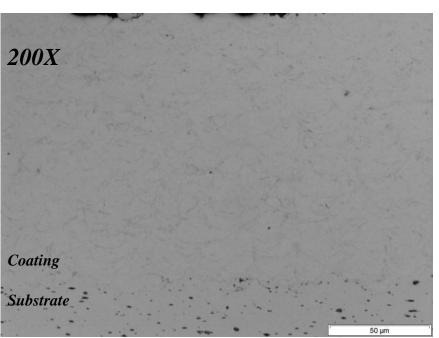


Increasing Gas Pressure









Alloy	Condition	Aging Temp (°F)	Time (Hrs)	Solutionizing Temp (°F)	Aging after Solutionizing Temp (°F)	Time (Hrs)	
AZ91C	-T5	335	16				
AZ91C	-T6			775	335 420	16 5-6	
AZ92A	-T5	500					
AZ92A	-T6			765	425	5	
ZE41A	-T5	625	2				

ZE41A-T5 Substrate Temperature Recorded at 163.4°C (326.1°F)

T5 means articially aged

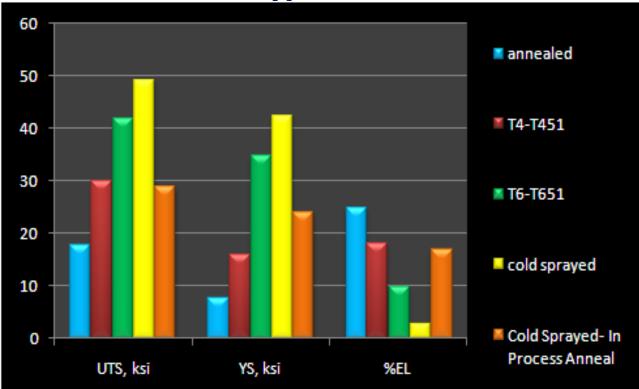
T6 means solution heat treated and artifically aged

M. M. Avedesian, Hugh Baker, "Magnesium and magnesium alloys", Edition: 2 - 1999, ASM International, pgs 78-79.





Wrought versus Cold Spray 6061



6061 Condition	Source	UTS, ksi	YS, ksi	%EL
annealed	1	18	8	25
T4, T451	2	30	16	18
T6, T651	2	42	35	10
cold sprayed (CS)	3	49.3	42.5	3
CS- In process anneal	3	29.0	24.0	17

Key
T4, T451- Solution heattreated and naturally aged to
a substantially stable
condition. Temper -T451
applies to products stressrelieved by stretching.<sup>2</sup>

T6, T651- Solution heattreated and then artificially aged, Temper -T651 applies to products stress-relieved by stretching.<sup>2</sup>

In Process Anneal- 640°F for 10 to 12 Hours

<sup>1</sup>Matweb

Alcoa.com

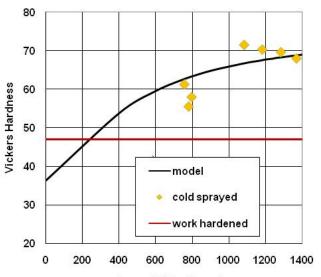
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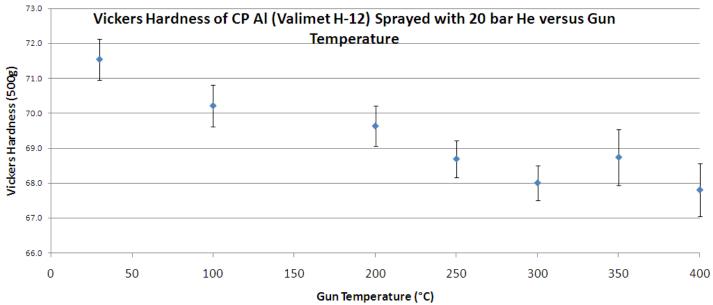
<sup>3</sup>Microtensile Test by Aaron Nardi at <u>UTRC</u> of ARL Cold Spray Block



# Technical Progress CP-Al Hardness



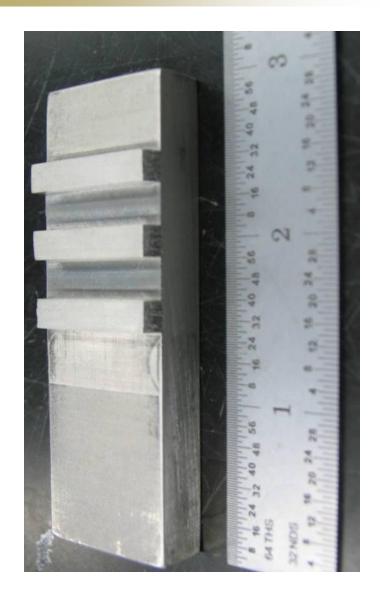


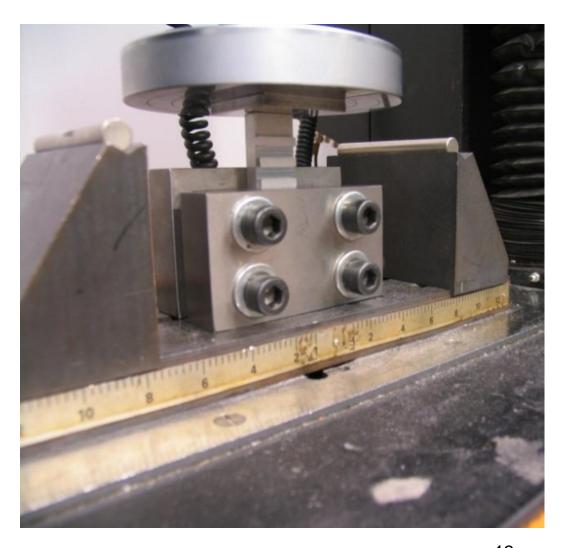




# Triple Lug Shear Test



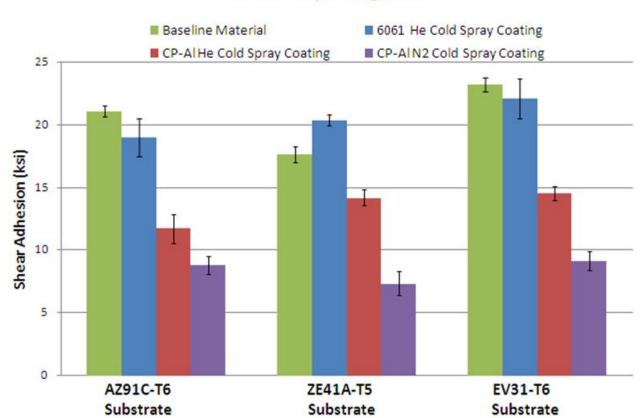




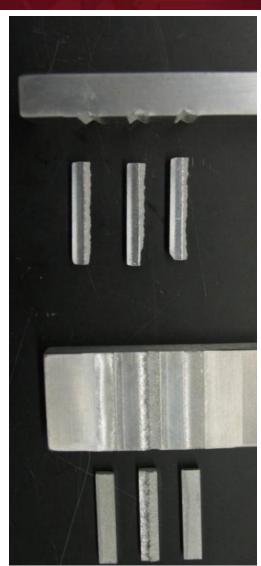




#### **ESTCP Triple Lug Data**



- ➤ Test Description: Thick coating is deposited and machined into three lugs (3/16" x 1") and then tested in compression
- > 7 out of 12 6061 on ZE41A-T5 samples failed within the Mg



6061/ZE41A+T6





## Bond Bar Adhesion (ASTM C633)



Substrate	Coating System	Averge Thickness (in)	Average Max Tensile Stress (PSI)	Stdev. Tensile Stress (PSI)	95% Confidence Tensile (PSI)	Observed Failure Mechanism
ZE41A-T5	6061 He	0.0134	11052	808	560	100% Glue
	CP-AI He	0.0197	12069	597	370	100% Coating Adhesion
	CP-AI N <sub>2</sub>	0.0228	10400	846	677	100% Coating Adhesion

**ZE41A-T5** 

**AZ91C-T6** 

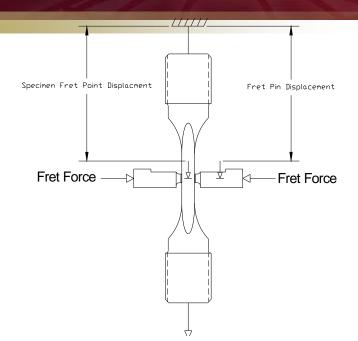
EV31-T6





#### Fretting Fatigue Setup at UTRC





Fretting rig pressure = 848 psi

Projected area fretting stress = 5 ksi (34 Mpa)

Fretting pin load = 167 lb

Fretting slip amplitude = ±0.001 inches (±25 microns)

Range of max axial test loads = 443 - 2955 lbs
Range of max axial test stress = 3 - 20 ksi
Range of lives = 32,000 - 10 million (runout)
Phasing = in phase with fret slip increasing at max axial

Pin Type = 0.206 diameter 4340 steel with

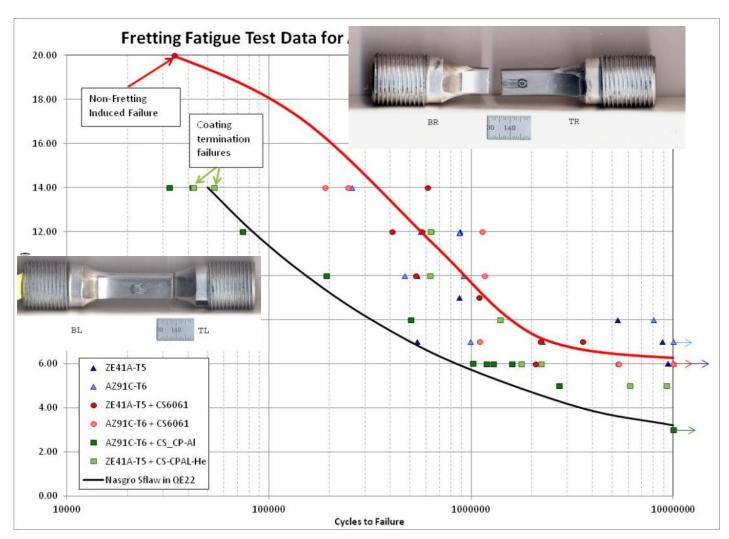
**ARL Fretting Fatigue Test Matrix** 

Specimen Base Material	Counterface Pin Material	Coating	# of Specimens Tested	Specimens Remaining
Wiateriai	iviaterial	None	10	∩ Nemaining
AZ91C-T6		6061 using Helium	9	0
	4130, 30-35 HRC ,	CP-Al using Nitrogen	11	0
ZE41A-T5	Cadmium plated	None	11	0
		6061 using Helium	9	0
		CP-Al using Nitrogen	9	0



# RDECOM Cold Spray Repair Fretting Fatigue





Slide Courtesy of Aaron Nardi, United Technologies Research Center



#### Fretting Fatigue Summary



#### **Test Results and Conclusions**

- AZ91C-T6 and ZE41A-T5 with no coating applied exhibited a 10 million cycle life of approximately 6.2 ksi
- Both Magnesium alloys with cold sprayed 6061 applied by helium exhibited a 10 million cycle life of approximately 5.3 ksi
- ZE41A-T5 with cold sprayed CP Aluminum applied using helium exhibited a 10 million cycle life of approximately 4.9 ksi
- AZ91C-T6 magnesium with cold sprayed CP aluminum using nitrogen exhibited a 10 million cycle life of approximately 3.3 ksi
- Fretting failures on baseline materials matched the expected fracture pattern
  - The cracking from top edge of fretting scar
  - Coating cracks propagated without changing direction at the interface suggesting a good bond and higher modulus

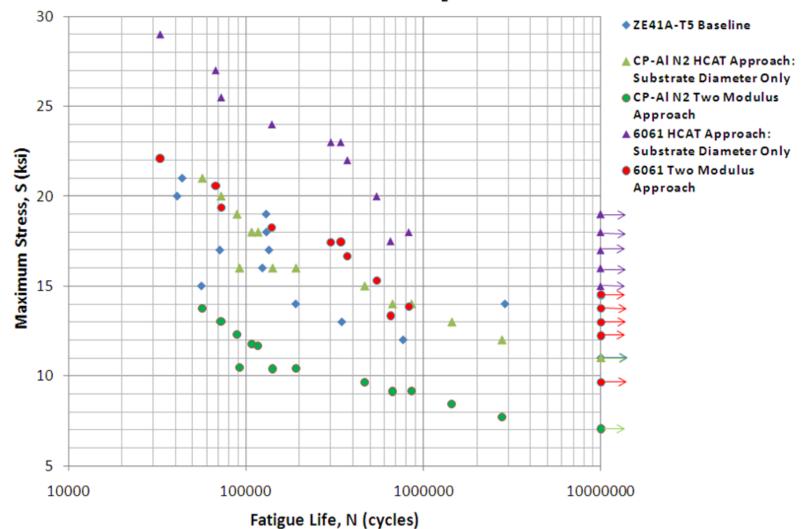
Slide Courtesy of Aaron Nardi, United Technologies Research Center



#### RR Moore Fatigue



#### ESTCP RR Moore Data: 6061 and CP-Al N<sub>2</sub> on ZE41A-T5

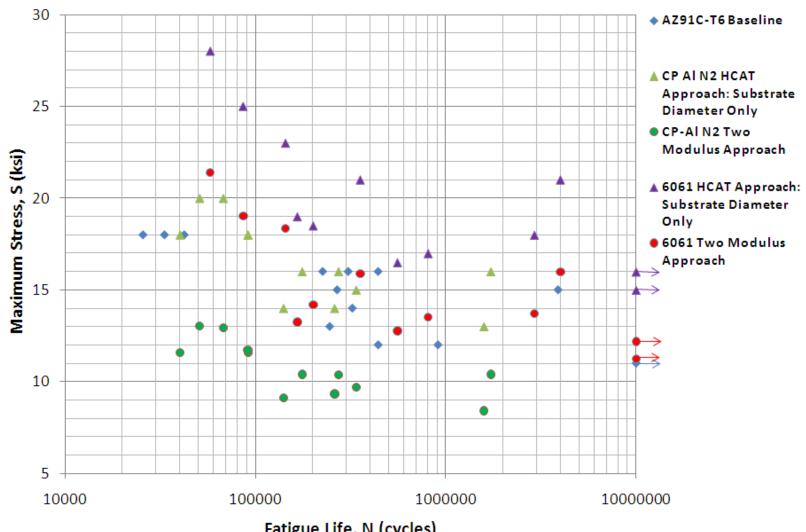




#### RR Moore Fatigue



#### ESTCP RR Moore Data: 6061 and CP-Al N<sub>2</sub> on AZ91C-T6



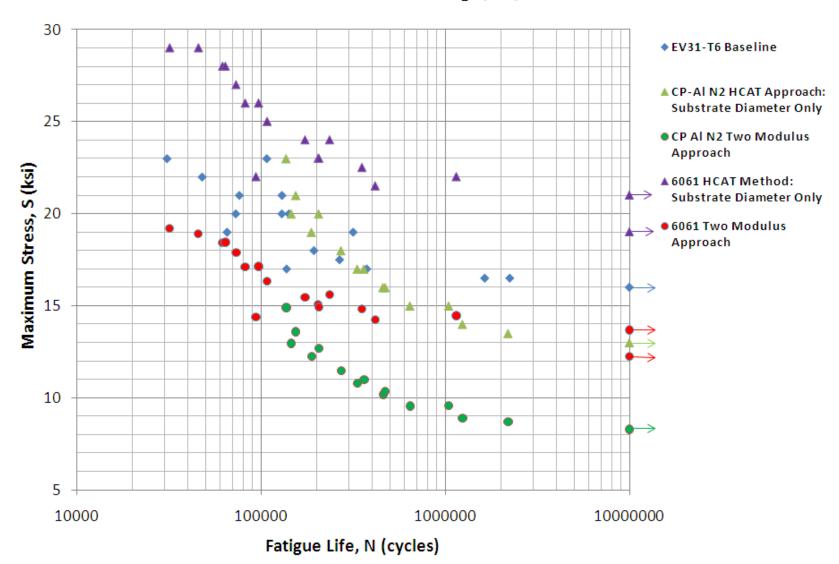
Fatigue Life, N (cycles)



#### RR Moore Fatigue

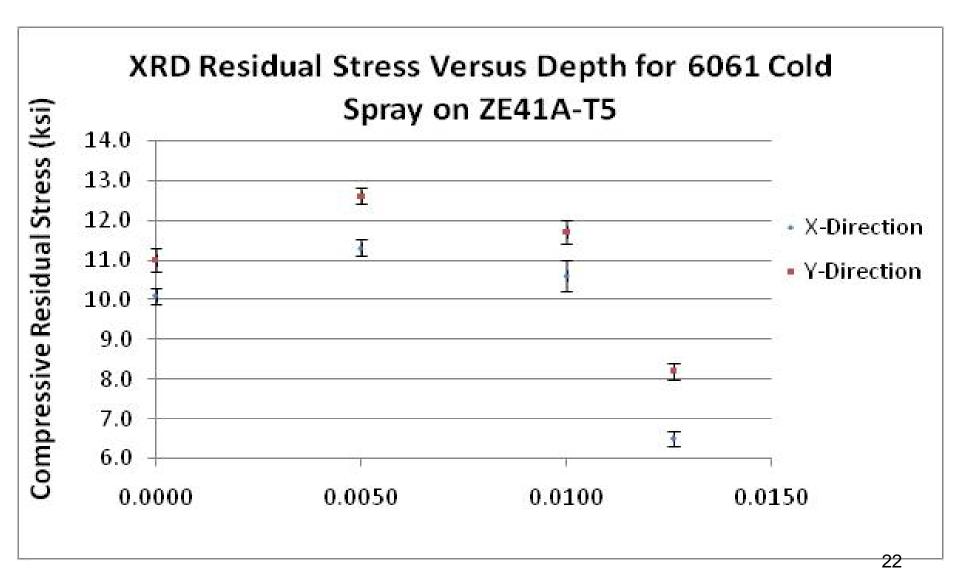


#### ESTCP RR Moore Data: 6061 and CP-Al N<sub>2</sub> Sprayed with N2 on EV31-T6





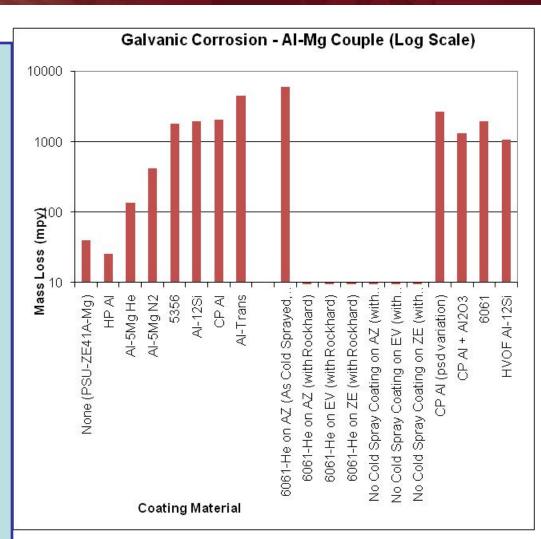








- Un-scribed ASTM B117
  - > CP-Al went well (7000 hours at Army and 1000 hours at PSU)
  - ➤ 6061 went 7000 hours at Army and will be retested at PSU due to thin spots
- > Scribed ASTM B117
  - > 1000 hours through top coat but 24 hours through to substrate. On par with HVOF Al-12Si
- GM9540 Scribed- Sprayed
- Galvanic Corrosion (G71)
- Crevice Corrosion (G78)- No Crevice mechanism
- > Beach Corrosion- Undergoing testing



\*vs uncoated ZE41

-Cd plated steel specimens are currently being <sub>23</sub> fabricated for comparison



# Sump Qualification



#### Sump Assembly Main Module-Main Gearbox Repair



Substrates: ZE41A & AZ91C Magnesium Coating Material: CP-Aluminum and/or 6061 Al

## RDECOM 2010 Summary at a Glance



- Cold Spray Coating Parameters Optimized at ARL
- > All Specimens from the JTP have been sprayed by ARL
- Testing is nearing completion for all Mechanical and Corrosion Specimens- All Partners (UTRC, Westmoreland, PSU, FRCEast, NAVAIR, ARL)
  - Unscribed B117- 7000 hours
  - Fretting Fatigue- Acceptable for He coatings
  - RR Moore- CP-Al N2 for non-structural, 6061 potential for structural repair
- Cold spray system at FRCEast is operational and ready for limited production